

## Full paper

## Flexible PET/EVA-based piezoelectret generator for energy harvesting in harsh environments

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## ABSTRACT

Stable and repeatable operation is paramount for practical and extensive applications of all energy harvesters. Herein, we develop a new type of flexible piezoelectret generator, which converts mechanical energy into electricity consistently even under harsh environments. Specifically, the generator, with piezoelectric coefficient ( $d_{33}$ ) reaching  $\sim 6300$  pC/N, had worked stably for continuous  $\sim 90000$  cycles, and the generator pressed by a human hand produced load peak current and power up to  $\sim 29.6$   $\mu$ A and  $\sim 0.444$  mW, respectively. Moreover, the capability to steadily produce electrical power under extreme moisture and temperature up to  $70$   $^{\circ}$ C had been achieved for possible applications in wearable devices and flexible electronics.

## 1. Introduction

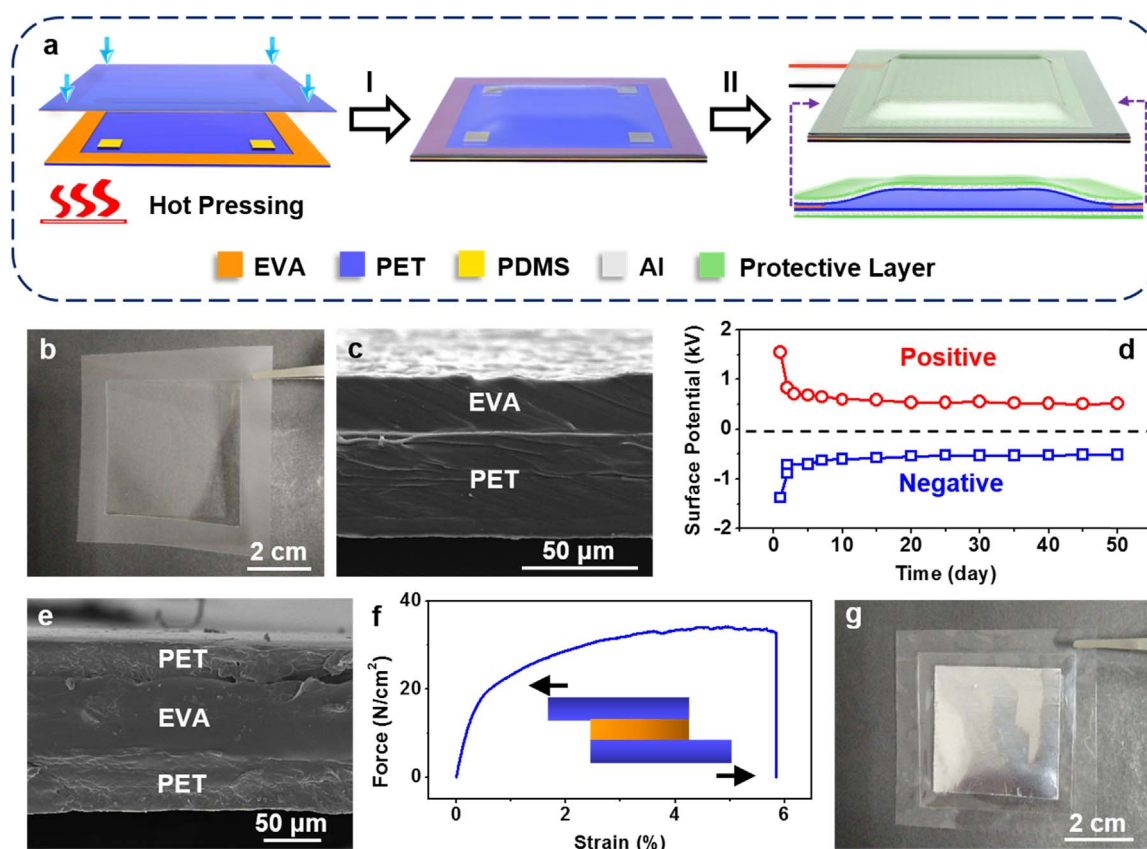
With the rise of intelligent wearable electronics, energy harvesters converting ambient mechanical energy into electricity have attracted much attention, which is not only because the energy source (*e.g.* human body movement, airflow, sound vibration, water waves *etc.*) ubiquitously exists in ambient background and is free, but also because the converting energy could enable these electronics to be functional indefinitely, thereby reducing the dependence on battery power [1–3]. Recently, flexible generators based on different working mechanism mainly including piezoelectric [4,5], electromagnetic [1,6] and electrostatic effect [3,7–17] have been successfully demonstrated with typical applications in mobile health care [8,13], human-machine interaction [9,14], wireless communication [15] and self-charging cells [10,11], *etc.* Among these generators, flexible electrostatic generators like triboelectric generators [3,7–12] and electret generators [13–17], have obtained more interests due to their simple fabrication process, high conversion efficiency and environmentally friendly without chemical processing. However, the output properties and stability of those generators are mainly determined by the surface surplus charges [15,18,19], which will be neutralized, once exposed to the moist air atmosphere, impairing the output performance of generators [20–22]. Thus, well encapsulation of these electrostatic generators is required to endure long-term exposure to harsh environments. Previously, Guo

et al. demonstrated a water-proof triboelectric generator that could be driven by the water flow [23], and Lee et al. had developed a fully packaged triboelectric sensors array for mapping the distribution of foot produced pressure [24]. However, the additional packaging material would add volume and reduce the flexibility of the generators [15,20]. New strategy with minimum packaging materials and low impact on the flexibility should be considered for flexible generators operating under harsh environments.

Flexible piezoelectret, known of high piezoelectric coefficient ( $d_{33}$ ), light-weight and low-cost, *etc.*, has extensive transducer applications, such as energy harvesters [25–28] and loudspeakers [29]. Since the electric dipole-like charges are produced inside the materials [25], the piezoelectret generators, one kind of electrostatic generators, have the potential to be excellent energy harvester candidates that still can perform well in harsh environments. In this work, we present a new type of flexible piezoelectret generator based on the polyethylene terephthalate (PET) electret film and the ethylene vinyl acetate copolymer (EVA) adhesive layer *via* a hot-pressing method. The corona charging technique was used to generate megascopic electric dipoles inside a big air bubble of the generator. Mechanical push and release the generator will change the dipole moments of the electric dipoles and alter the electrostatic induction intensity to generate alternating electricity, with  $d_{33}$  coefficient reaching  $\sim 6300$  pC/N and stable outputs for continuous  $\sim 90000$  operations. Experimentally, the

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**Fig. 1.** Fabrication of the flexible PET/EVA-based piezoelectric generator. (a) Schematic diagram showing the fabrication steps of the generator, (I) hot pressing and corona charging; (II) placing and adhesion of the electrodes and protective layers. (b) An optical photo of the EVA/PET laminated film. (c) Cross-section view SEM image of the EVA/PET laminated film. (d) Surface potential versus time curves for the PET electret with positive and negative corona charging, showing little decay after the first 5 days. (e) Cross-section view SEM image of the PET/EVA/PET laminated film. (f) Mechanical shear testing result of the PET/EVA/PET laminated film. (g) An optical photo showing a fabricated generator.

generator pressed by a human hand produced load peak current and power up to  $\sim 29.6 \mu\text{A}$  and  $\sim 0.444 \text{ mW}$ , respectively. Moreover, the most prominent advantage of this generator is the remarkable output stability under harsh environments of extreme moisture and temperature up to  $70^\circ\text{C}$ , indicating that the generator may be suitable for wearable energy harvesting and used in other harsh environments.

## 2. Results and discussion

### 2.1. Fabrication of the flexible PET/EVA-based piezoelectric generator

The detailed fabrication steps of the flexible PET/EVA-based piezoelectric generator are schematically given in Fig. 1a and Fig. S1. The raw material was the flexible  $\sim 45 \mu\text{m}$ -thick PET electret film with the  $\sim 25 \mu\text{m}$ -thick and ring-shape EVA adhesive layer at the boundary, which was defined as the EVA/PET laminated film (Fig. 1b). The cross-section view scanning electron microscope (SEM) image (Fig. 1c) clearly shows the EVA/PET laminated structure. The surface morphology of the PET electret film was investigated by atomic force microscope (AFM), indicating the PET surface roughness varied from  $\sim -82$  to  $\sim 78 \text{ nm}$  (Fig. S2). In theory, the rough surface morphology is helpful to capture more surplus charges. The charges capturing ability of the PET electret film was studied *via* the corona charging method [15], as indicated in Fig. S3. In this work, two PET electret films were charged with positive and negative high voltages (values of 20 and  $-20 \text{ kV}$ ), respectively, and then the corresponding surface potential versus time curves were measured (Fig. 1d). It's found that the surface potential for positive and negative charging still maintained at about 0.52 and  $-0.50 \text{ kV}$  after 50 days, respectively. These results indicate that the

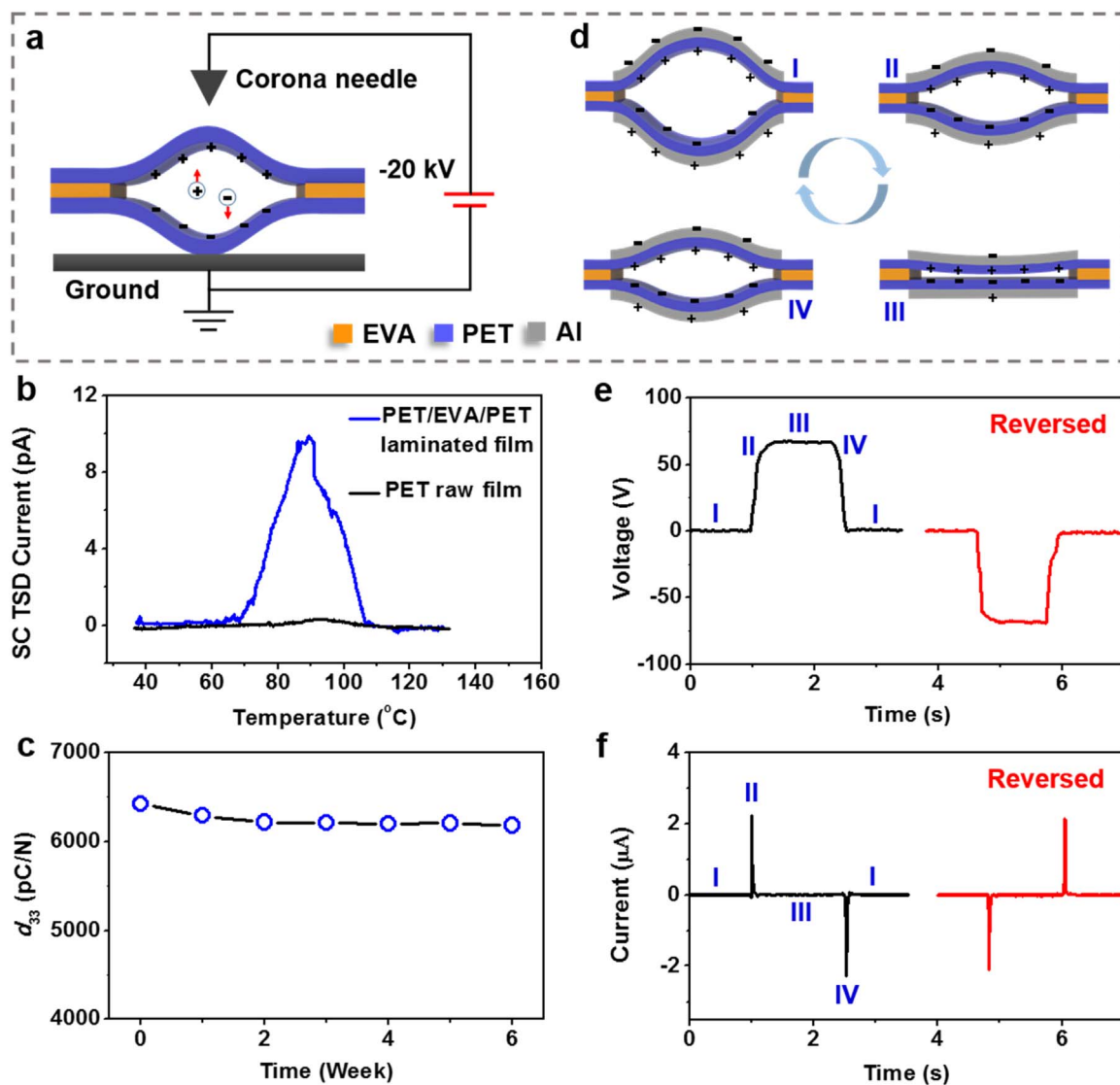
PET electret film is an excellent electret material, with the ability to capture and maintain both positive and negative surplus charges for a long time.

The fabrication steps began with fixing four polydimethylsiloxane (PDMS) spacers (size of  $0.5 \times 0.25 \text{ cm}^2$ , thickness of 1 mm) on four corners of the EVA/PET laminated film (Fig. S1-I and Fig. S4a). Subsequently, another EVA/PET laminated film placed at the top was bonded to the laminated film with spacers *via* a hot-pressing method (Fig. 1-I, Fig. S1-II), forming the PET/EVA/PET laminated film with an arch-shaped air bubble with the height of 0.5–1 mm (Fig. S4b). The cross-section view SEM image indicates that the two EVA/PET laminated films were bonded tightly (Fig. 1e). Moreover, the PET/EVA/PET laminated film could stand the shearing force up to  $\sim 33 \text{ N/cm}^2$  before separation, indicating the strong mechanical bonding characteristics (Fig. 1f).

The as-fabricated PET/EVA/PET laminated film was then corona charged, in order to generate megascopic electric dipoles inside the air bubble (Fig. S1-III) [26]. In the next step, aluminum (Al) adhesive tape (thickness of  $\sim 100 \mu\text{m}$ ) was covered on two outside surfaces of the charged PET/EVA/PET laminated film, as the electrodes (Fig. S1-IV). Lastly, two protective layers (water proof tape, thickness of  $\sim 50 \mu\text{m}$ ) were covered on two Al electrodes (Fig. S1-V), forming a PET/EVA-based flexible electret generator with effective area of about  $\sim 4 \times 4 \text{ cm}^2$  (Fig. 1-II and Fig. 1g).

### 2.2. Working mechanism of the PET/EVA-based flexible piezoelectric generator

By virtue of the megascopic electric dipoles inside the air bubbles, piezoelectric materials have the piezoelectric-like property as the



**Fig. 2.** Working mechanism of the flexible PET/EVA-based piezoelectric generator. (a) Schematic diagram indicating the corona charging method. (b) Short circuit TSD current measurement results for the PET/EVA/PET laminated film and PET raw film. (c) The characterized  $d_{33}$  coefficient for the generator placed in the indoor atmosphere for 6 weeks. (d) Schematic diagram indicating the electricity generation of the generator when it is at (I) original, (II) compressing, (III) equilibrium and (IV) releasing states, respectively. (e) Open-circuit voltages and (f) short-circuit currents for the generator when it was forward-connected and reverse-connected to the measurement system, respectively.

traditional piezoelectric materials, similar to lead zirconate titanate (PZT), zinc oxide (ZnO) and polyvinylidene fluoride (PVDF), etc [25,30,31]. Herein, the corona charging method was used to generate electric dipoles inside the air bubble of the PET/EVA/PET laminated film before the two electrodes were added on the outer surfaces, as shown in Fig. 2a. Specifically, high voltage up to  $-20$  kV was applied on the corona needle for about 3 min, with samples placed about 5 cm below the needle tip. Under the strong electric field intensity, the air in the air bubble was broken down to generate ionic charges with both polarities. The positive and negative ionic charges were driven by the electric field, and captured by the upper and lower inner PET surfaces, respectively. As a result, the air bubble with charged PET inner surfaces worked as megascopic electric dipoles.

The short circuit thermally stimulated discharge (TSD) method was employed to verify the existence of electric dipoles (Fig. S5). Specifically, our laminated film and PET raw film were corona charged first, and then two outer surfaces were covered by Al electrodes. The samples were heated in a thermal chamber with a temperature rising rate of  $3$  °C/min, and the induced current curves were recorded *in-situ* by an electrometer. If there are electric dipoles, measurable electrical current peak in the heating process can be measured. As indicated in

Fig. 2b, the measured current curve of the PET/EVA/PET laminated film consisted of a current peak started at about  $70$  °C and ended at about  $110$  °C, with the maximum peak value located at about  $90$  °C. The influences from the potential shape changes of the air bubble were negligible as no visible output currents were measured before  $70$  °C. In comparison, no significant current peak was observed in the short circuit TSD current curve of the PET raw electret film.

To measure the quasi-static piezoelectric  $d_{33}$  coefficient, a generator was operated by a give force  $F$  and the corresponding short-circuit output current was recorded (Fig. S6a). The value of transferred charges  $Q$  was achieved by integrating the current over time (Fig. S6b), and the  $d_{33}$  coefficient can be calculated [26]:

$$d_{33} = Q/F \quad (1)$$

The  $d_{33}$  coefficient of our generator reached  $\sim 6300$  pC/N, which was significantly larger than that of generators based on traditional cellular polypropylene (PP) piezoelectret film (Fig. 2c) [26,32]. This outstanding piezoelectric property is attributed to the excellent charges capturing ability of PET electret and low elastic modulus of the air bubble structure. Moreover, the stability of  $d_{33}$  coefficient was investigated by placing the generator in indoor atmosphere for weeks and it

maintained in a narrow range around the original value for 6 weeks, as indicated in Fig. 2c.

Based on above piezoelectric-like behavior, Fig. 2d schematically illustrates the power generating processes of the generator. At any states, the megascopic electric dipoles will generate induced charges on the top and bottom Al electrodes, and the charge density on the electrode ( $\sigma_e$ ) is decided by the following equation [27]:

$$\sigma_e = -\epsilon_0 \epsilon E = \frac{\epsilon \sigma_0}{\left(\frac{D_1}{D_2} + \epsilon\right)} \quad (2)$$

where  $\epsilon_0$  and  $\epsilon$  are the dielectric constant of air and relative dielectric constant of PET, respectively.  $E$  is the electric field in the PET layer and  $\sigma_0$  represents the charge density captured by the PET inner surface.  $D_1$  is the thickness of PET layer and  $D_2$  is thickness of air bubble or the dipole moments of the megascopic electric dipoles. In our case,  $\epsilon_0$ ,  $\epsilon$ ,  $E$ ,  $\sigma_0$ , and  $D_1$  are constants, and  $\sigma_e$  is affected by  $D_2$ .

Fig. 2d-f show a non-sinusoidal excitation (hand pressing motion) of the generator with the resulting open-circuit voltage response and short-circuit current response. In the original state (Fig. 2d-I), the electrical potential between the two electrodes are in equilibrium state, and no open-circuit voltage or short-circuit current can be observed (Fig. 2e-I and Fig. 2f-I). When the generator is compressed (Fig. 2d-I to III), during the very short state II,  $D_2$  decreases and the charge densities on the top and bottom electrodes also decrease. The open circuit voltage curve increases in the whole compressing process (Fig. 2e-I to III). The short circuit current curve increases to positive peak value (Fig. 2f-I to II) and then drops to zero (Fig. 2f-II to III), resulting a sharp positive current peak. As the compression state maintains (Fig. 2d-III), a new equilibrium is established. The open-circuit voltage keeps at the highest value (Fig. 2e-III) and the short circuit current keeps at zero (Fig. 2f-III). It is noted that most of the surplus charges will not be neutralized when the two PET layers are

contacted with each other, which is benefit by the rough surface morphology of the PET (Fig. S2). If the generator is released (Fig. 2d-III to I, during the very short state IV),  $D_2$  increases because of the mechanical elasticity of the generator. The charge density on both electrodes will increase. The open-circuit voltage drops from highest value to zero (Fig. 2e III to I). The short circuit current increases to negative peak value (Fig. 2f-III to IV) and then drops to zero (Fig. 2f-IV to I), resulting a sharp negative current peak. At last, the electrical potential between the two electrodes become in equilibrium state again.

In general, the basic working mechanism of the generator is the electrostatic induction effect caused by the megascopic electric dipoles. Compressing and releasing the generator will change the dipole moments of the electric dipoles. Thus, the electrical potential between the two electrodes are changed, and the alternating electricity is generated. Switching polarity tests were also carried out to confirm that the measured output signals are generated from the generator rather than from the artifacts of the measurement system (given in the right side of Fig. 2e and f).

### 2.3. Electrical output properties of the flexible PET/EVA-based piezoelectret generator

The electrical outputs of the flexible PET/EVA-based piezoelectret generator were carefully investigated by periodically compressing and releasing at controlled pressure and sinusoidal frequency. Typically, the generator was attached to a force meter, which was tightly fixed onto an x-y-z mechanical stage.

By virtue of the large piezoelectric  $d_{33}$  coefficient, the output properties of our generator were excellent. Under given applied pressure of 6.67 kPa and sinusoidal frequency of 5 Hz, the load peak current and power density of the generator with different external

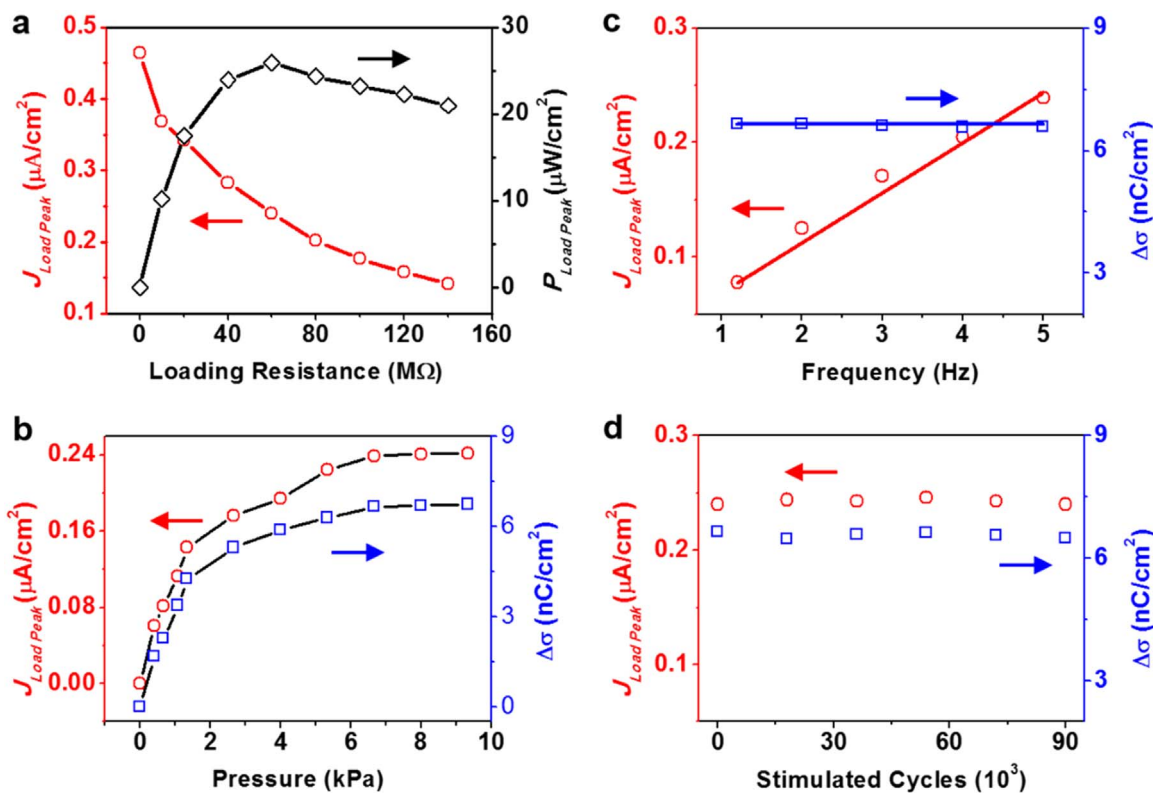


Fig. 3. Electrical outputs of the flexible PET/EVA-based piezoelectret generator. (a) Load peak current and power density of a generator with respect to different load resistances, under given applied pressure of 6.67 kPa and sinusoidal frequency of 5 Hz. (b) Load peak current and transferred charge density for a generator with respect to given applied frequency of 5 Hz and different applied pressure. (c) Load peak current and transferred charge density for a generator respect to given applied pressure of 6.67 kPa and different applied frequency. (d) Load peak current and transferred charge density for a generator for continuous operations of 90000 cycles, under given applied pressure and frequency of 6.67 kPa and 5 Hz.

resistors were measured (Fig. 3a). The maximum load peak power density reached  $\sim 25.923 \mu\text{W}/\text{cm}^2$ , when the corresponding load peak current density and load resistance were  $\sim 0.241 \mu\text{A}/\text{cm}^2$  and  $60 \text{ M}\Omega$ , respectively. It should be noted that unless otherwise specified, the load resistance is  $60 \text{ M}\Omega$  for optimal outputs for the prototype system.

The load peak current density and corresponding transferred charge density ( $\Delta\sigma$ ) for the generator under given applied frequency of 5 Hz and different applied pressure is given in Fig. 3b. It's found that when the applied pressure was less than 1.33 kPa, the load peak current density increased approximately linearly. As the applied pressure increased to be higher than 1.33 kPa, the load peak current density increased approximately linearly too, with a smaller increasing rate. The variation tendency of the  $\Delta\sigma$  was similar to that of the load peak current density, which was divided to two regions. These output behaviors are similar to the “vertical contact-separation mode triboelectric generator” [33]. The load peak current density and  $\Delta\sigma$  reached  $\sim 0.239 \mu\text{A}/\text{cm}^2$  and  $\sim 6.648 \text{ nC}/\text{cm}^2$ , respectively, when the applied pressure reached 6.67 kPa. By continuously increasing the applied pressure, the peak current and corresponding transferred charge density of our generator tended to be saturated, as the air bubble was completely compressed.

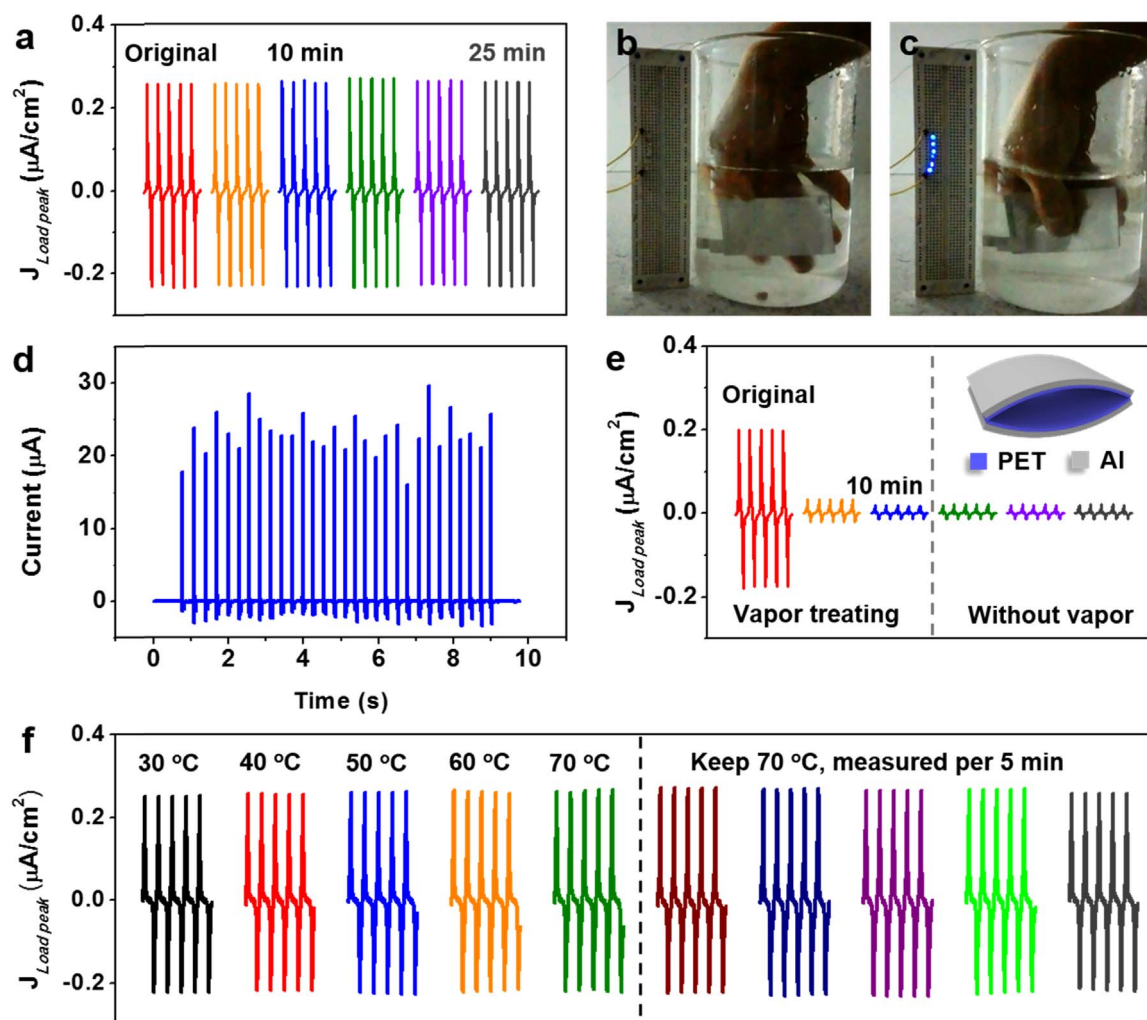
Furthermore, the load peak current density and  $\Delta\sigma$  increased step

by step under given applied pressure of 6.67 kPa and different applied frequency, from  $\sim 0.077 \mu\text{A}/\text{cm}^2$  at 1.2 Hz to  $\sim 0.237 \mu\text{A}/\text{cm}^2$  at 5 Hz. However, the  $\Delta\sigma$  almost kept at a constant value of  $\sim 6.650 \text{ nC}/\text{cm}^2$  for different applied frequency (Fig. 3c). According to the above results, the load peak current density of the generator is related to both of the applied pressure and frequency, and the  $\Delta\sigma$  is only related to applied pressure.

The output stability performance of the generator was studied by pressing and releasing for continuous  $\sim 90000$  cycles, under given applied pressure and frequency of 6.67 kPa and 5 Hz, respectively. As indicated in Fig. 3d, both of the load peak current density and  $\Delta\sigma$  remained at the constant values of  $\sim 0.245 \mu\text{A}/\text{cm}^2$  and  $\sim 6.645 \text{ nC}/\text{cm}^2$ . This remarkable stability performance is attribute to the excellent charges capturing ability of PET electret and good flexibility and elasticity of the generator.

#### 2.4. Stability of the flexible PET/EVA-based piezoelectret generator under harsh environments

As the megascopic electric dipoles exist inside the flexible PET/EVA-based piezoelectret generator and the electrodes are well protected, this generator has the great potential in harvesting mechanical



**Fig. 4.** Output stability characterizations of the flexible PET/EVA-based piezoelectret generator under harsh environments. (a) Current outputs of the generator under the high water vapor environment, under given applied pressure of 6.67 kPa and sinusoidal frequency of 5 Hz. Optical photos for (b) the generator under water and (c) 6 blue LEDs lit up by hand pressing the generator under water. (d) Current flowing through the LEDs when they were lit up. (e) Currents outputs for an arch-shaped generator under the high water vapor environment and the following without vapor environment, under given applied pressure and frequency of 6.67 kPa and 5 Hz. Insert in (e) showing the schematic diagram of the arch-shaped generator. (f) Current outputs for a flexible PET/EVA-based piezoelectret generator when the temperature increased from 30 °C to 70 °C and then kept at 70 °C, under given applied pressure and frequency of 6.67 kPa and 5 Hz.

energy under harsh environments. The stability of the generator under extreme moisture environment was investigated. Specifically, the generator was placed into a closed space full of water vapor and continuously operated under given applied pressure of 6.67 kPa and sinusoidal frequency of 5 Hz, respectively (Fig. S7). Typical load current curves generated by the generator in one second were recorded for every 5 min (Fig. 4a). The load peak current density varied between  $\sim 0.256 \mu\text{A}/\text{cm}^2$  and  $\sim 0.268 \mu\text{A}/\text{cm}^2$  for the whole 25 min of measurement. Moreover, the generator was soaked into water (Fig. 4b), and 6 blue LEDs connected in series were lit up by hand pressing the generator (Fig. 4c and Video 1). The turn-on threshold voltage of the 6 blue LEDs was  $\sim 15 \text{ V}$  (Fig. S8) and the highest peak current went through the LEDs was  $\sim 29.6 \mu\text{A}$  (Fig. 4d). Therefore, the generator generated an instantaneous output power of  $\sim 0.444 \text{ mW}$ . Above results indicated that our generator had the outstanding ability in converting the mechanical energy into electricity under the extreme moisture environment or even completely immersed in water.

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In comparison, an arch-shaped flexible generator (insert in Fig. 4e) based on PET electret film was also operated under the high water vapor environment. In this case, the surplus charges contacted with extreme moisture directly. The load peak current density dropped from  $\sim 0.197 \mu\text{A}/\text{cm}^2$  to  $\sim 0.0185 \mu\text{A}/\text{cm}^2$  after continuously operating for 10 min. Then, the generator was only operated for 3 s at each 5 min time interval after removing the vapor, the output current of the generator could not recover again (Fig. 4e).

The output performance of the flexible PET/EVA-based piezoelectret generator under different temperatures was characterized. A heater was used to control the temperature of the generator, which was continuously operated under the applied pressure and frequency of 6.67 kPa and 5 Hz (Fig. S9). As given in Fig. 4f, when the temperatures increased from  $30^\circ\text{C}$  to  $70^\circ\text{C}$ , the load peak current density only had relatively stable outputs between  $\sim 0.251 \mu\text{A}/\text{cm}^2$  and  $\sim 0.263 \mu\text{A}/\text{cm}^2$ . If the temperature was then kept at  $70^\circ\text{C}$  for 25 min, the output currents remained stable. However, higher temperature can cause the loss of the megascopic electric dipoles inside the generator based on the short circuit TSD measurement result (Fig. 2b). As such, the output performance of the generator would reduce (Fig. S10).

### 3. Conclusions

In summary, a new type of flexible piezoelectret generator based on EVA/PET laminated film was fabricated, in which megascopic electric dipoles were captured inside the air bubble. By changing the dipole moments of the electric dipoles, the generator converted mechanical energy into electricity effectively, with  $d_{33}$  coefficient reaching  $\sim 6300 \text{ pC/N}$ . Specifically, load peak current and corresponding peak power of  $\sim 29.6 \mu\text{A}$  and  $\sim 0.444 \text{ mW}$  were reached by hand pressing the generator, and stable outputs were achieved for  $\sim 90000$  continuous working cycles. More importantly, the generator had remarkable output stability under harsh environments with extreme moisture and temperature up to  $70^\circ\text{C}$ , indicating the feasibility for wearable energy harvesting. This study provides a new, simple and efficient strategy for designing robust and reliable flexible energy harvesting devices.

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### Appendix A. Supporting information

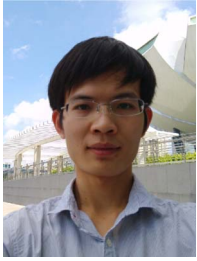
Supplementary data associated with this article can be found in the online version at doi:10.1016/j.nanoen.2017.05.034.

### References

- [1] A.D. Kuo, *Science* 309 (2005) 1686.
- [2] C. Chang, V.H. Tran, J. Wang, Y.-K. Fuh, L. Lin, *Nano Lett.* 10 (2010) 726.
- [3] F.-R. Fan, Z.-Q. Tian, Z.L. Wang, *Nano Energy* 1 (2012) 328.
- [4] L. Persano, C. Dagdeviren, Y. Su, Y. Zhang, S. Girardo, D. Pisignano, Y. Huang, J.A. Rogers, *Nat. Commun.* 4 (2013) 1633.
- [5] Y. Qi, M.C. McAlpine, *Energy Environ. Sci.* 3 (2010) 1275.
- [6] J.M. Donelan, Q. Li, V. Naing, J.A. Hoffer, D.J. Weber, A.D. Kuo, *Science* 319 (2008) 807.
- [7] Z.L. Wang, J. Chen, L. Lin, *Energy Environ. Sci.* 8 (2015) 2250.
- [8] J. Yang, J. Chen, Y. Su, Q. Jing, Z. Li, F. Yi, X. Wen, Z. Wang, Z.L. Wang, *Adv. Mater.* 27 (2015) 1316.
- [9] B.-U. Hwang, J.-H. Lee, T.Q. Trung, E. Roh, D.-I. Kim, S.-W. Kim, N.-E. Lee, *ACS Nano* 9 (2015) 8801.
- [10] A. Ramadoss, B. Saravanakumar, S.W. Lee, Y.-S. Kim, S.J. Kim, Z.L. Wang, *ACS Nano* 9 (2015) 4337.
- [11] H. Guo, M.-H. Yeh, Y.-C. Lai, Y. Zi, C. Wu, Z. Wen, C. Hu, Z.L. Wang, *ACS Nano* 10 (2016) 10580.
- [12] H. Kang, H. Kim, S. Kim, H.J. Shin, S. Cheon, J.-H. Huh, D.Y. Lee, S. Lee, S.-W. Kim, J.H. Cho, *Adv. Funct. Mater.* 26 (2016) 7717.
- [13] J. Zhong, Y. Zhang, Q. Zhong, Q. Hu, B. Hu, Z.L. Wang, *J. Zhou, ACS Nano* 8 (2014) 6273.
- [14] J. Zhong, H. Zhu, Q. Zhong, J. Dai, W. Li, S.-H. Jang, Y. Yao, D. Henderson, Q. Hu, L. Hu, *J. Zhou, ACS Nano* 9 (2015) 7399.
- [15] J. Zhong, Q. Zhong, G. Chen, B. Hu, S. Zhao, X. Li, N. Wu, W. Li, H. Yu, *J. Zhou, Energy Environ. Sci.* 9 (2016) 3085.
- [16] Y.S. Ko, F.A. Nüesch, D. Damjanovic, D.M. Opris, *Adv. Mater.* 29 (2016) 1603813.
- [17] T. Vu-Cong, C. Jean-Mistral, A. Sylvestre, *Smart Mater. Struct.* 22 (2013) 025012.
- [18] G.M. Sessler, *J. Electro.* 51 (2001) 137.
- [19] J. Zhong, Q. Zhong, F. Fan, Y. Zhang, S. Wang, B. Hu, Z.L. Wang, *J. Zhou, Nano Energy* 2 (2013) 491.
- [20] Y. Yang, H. Zhang, R. Liu, X. Wen, T.-C. Hou, Z.L. Wang, *Adv. Energy Mater.* 3 (2013) 1563.
- [21] L. Gu, N. Cui, J. Liu, Y. Zheng, S. Bai, Y. Qin, *Nanoscale* 7 (2015) 18049.
- [22] V. Nguyen, R. Yang, *Nano Energy* 2 (2013) 604.
- [23] H. Guo, Z. Wen, Y. Zi, M.-H. Yeh, J. Wang, L. Zhu, C. Hu, Z.L. Wang, *Adv. Energy Mater.* 6 (2016) 1501593.
- [24] K.Y. Lee, H.-J. Yoon, T. Jiang, X. Wen, W. Seung, S.-W. Kim, Z.L. Wang, *Adv. Energy Mater.* 6 (2016) 1502566.
- [25] S. Bauer, R. Gerhard-Multhaupt, G.M. Sessler, *Phys. Today* 57 (2004) 37.
- [26] N. Wu, X. Cheng, Q. Zhong, J. Zhong, W. Li, B. Wang, B. Hu, J. Zhou, *Adv. Funct. Mater.* 25 (2015) 4788.
- [27] W. Li, N. Wu, J. Zhong, Q. Zhong, S. Zhao, B. Wang, X. Cheng, S. Li, K. Liu, B. Hu, *J. Zhou, Adv. Funct. Mater.* 26 (2016) 1964.
- [28] B. Wang, C. Liu, Y. Xiao, J. Zhong, W. Li, Y. Cheng, B. Hu, L. Huang, *J. Zhou, Nano Energy* 32 (2017) 42.
- [29] J. Hillenbrand, G.M. Sessler, *Ferroelectrics* 472 (2014) 77.
- [30] X. Zhang, G.M. Sessler, Y. Wang, *J. Appl. Phys.* 116 (2014) 074109.
- [31] P. Pondrom, J. Hillenbrand, G.M. Sessler, J. Bös, T. Melz, *Appl. Phys. Lett.* 104 (2014) 172901.
- [32] Q. Zhong, J. Zhong, X. Cheng, X. Yao, B. Wang, W. Li, N. Wu, K. Liu, B. Hu, *J. Zhou, Adv. Mater.* 27 (2015) 7130.
- [33] L. Lin, Y. Xie, S. Wang, W. Wu, S. Niu, X. Wen, Z.L. Wang, *ACS Nano* 7 (2013) 8266.

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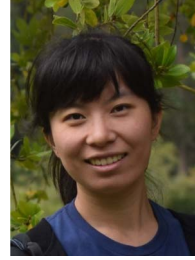
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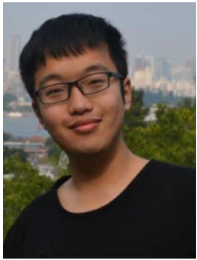
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